

Europäisches Patentamt
European Patent Office
Office européen des brevets



(11)

EP 1 365 441 A1

(12)

EUROPEAN PATENT APPLICATION

(43) Date of publication:
26.11.2003 Bulletin 2003/48

(51) Int Cl.7: **H01L 21/00**, B08B 7/00,
G03F 7/42, C11D 11/00,
C11D 7/32

(21) Application number: 03011130.6

(22) Date of filing: 22.05.2003

(84) Designated Contracting States:
**AT BE BG CH CY CZ DE DK EE ES FI FR GB GR
HU IE IT LI LU MC NL PT RO SE SI SK TR**
Designated Extension States:
AL LT LV MK

- Iijima, Katsuyuki, Kobe Corporate Research Lab.
Nishi-ku, Kobe-shi, Hyogo 651-2271 (JP)
- Yoshikawa, Tetsuya, Takasago Works
Takasago-shi, Hyogo 676-8670 (JP)
- Peters, Darry W.
New Jersey 08886 (US)

(30) Priority: 23.05.2002 US 152782

(71) Applicant: **Kabushiki Kaisha Kobe Seiko Sho
(Kobe Steel, Ltd.)
Kobe-shi, Hyogo 651-8585 (JP)**

(74) Representative: **Müller-Boré & Partner
Patentanwälte
Grafinger Strasse 2
81671 München (DE)**

(72) Inventors:
• **Masuda, Kaoru, Kobe Corporate Research Lab.
Nishi-ku, Kobe-shi, Hyogo 651-2271 (JP)**

(54) **Process and composition for removing residues from the microstructure of an object**

(57) A process for removing residues from the microstructure of an object is provided, which comprises steps of preparing a remover including carbon dioxide, an additive for removing the residues and a co-solvent dissolving the additive in said carbon dioxide at a pres-

surized fluid condition; and bringing the object into contact with the remover so as to remove the residues from the object. A composition for removing residues from the microstructure of an object is also provided.

EP 1 365 441 A1

Description

[0001] The present invention relates to a process and a composition for removing residues from the microstructure of an object. The present invention specifically relates to a process and a composition for removing residues, such as resists, generated during a semiconductor manufacturing process from a semiconductor wafer surface having a fine structure of convex and concave portions.

[0002] It is required as one step in manufacturing a semiconductor wafer to remove residues, such as photoresists, UV-hardened resists, X-ray hardened resists, ashed resists, carbon-fluorine containing polymer, plasma etch residues, and organic or inorganic contaminants from the other steps of the manufacturing process. The dry and wet removal methods are commonly used. In the wet removal method, the semiconductor wafer is dipped in an agent, such as a water solution, including a remover to remove residues from the surface of semiconductor wafer.

[0003] Recently, supercritical carbon dioxide is used as such an agent because of its low viscosity and high diffusivity. According to such properties, cleaning with supercritical carbon dioxide provides several advances in the treatment of microstructures, such as high penetration into small areas between microstructures and successfully drying microstructures because of non liquid-liquid interface in the supercritical phase.

[0004] However, supercritical carbon dioxide is not enough by itself to remove several residues from the surface of the semiconductor wafer. To resolve this problem, several additives to supercritical carbon dioxide are proposed. As described in the Japanese unexamined patent publication No. 10-125644, methane or surfactant having CF_x group is used as an additive to supercritical carbon dioxide. In Japanese unexamined patent publication No. 8-191063, dimethylsulfoxide or dimethyl-formamide is used as such an additive. However, based on the inventors' studies, these additives are not always effective for removing residues. Especially, when the cleaning object is like a wafer which consists of low dielectric constant materials, the quality of such wafer decreased after treatments by such process using alkaline compounds and water. This might be occurred because basic compounds and water caused damages on low dielectric constant materials, especially on materials having dielectric constant lower than 4. (hereinafter referred to as low-k materials) Thus, the present invention is objected to provide a novel and effective cleaning without significant damage to the low-k materials.

[0005] An object of the present invention is, therefore, to provide a process and a composition for effectively removing residues from the microstructure of an object without significant damages to the low-k materials.

[0006] According to the present invention, a process is provided for removing residues from the object, which comprises steps of preparing a remover including carbon dioxide, an additive for removing the residues, an inhibitor for protecting low-k damage and a co-solvent for dissolving said additive in said carbon dioxide at a pressurized fluid condition, and bringing the object into contact with said remover so as to remove the residues from the object.

[0007] A composition is further provided for removing residues from the object, which comprises carbon dioxide, a fluoride containing additive, a co-solvent or mixture of co-solvents capable of dissolving the fluoride containing additive, and an inhibitor.

[0008] The foregoing and additional features and characteristics of the present invention will become more apparent from the following detailed description considered with reference to the accompanying drawings in which like reference numerals designate like elements and wherein:

FIG. 1 is a schematic diagram of an apparatus for removing residues in accordance with the present invention.

[0009] The present invention is applied to the microstructure of an object, e.g., a semiconductor wafer having a fine structure of convex and concave portions on its surface, and a substrate made of a metal, plastic or ceramic which forms or remains continuous or non-continuous layer of materials different therefrom.

[0010] First, said remover used in this invention is described. It includes carbon dioxide, an additive for removing the residues, an inhibitor for suppressing residues and a co-solvent for dissolving said additive and said inhibitor in said carbon dioxide at a pressurized fluid condition. The pressurized carbon dioxide has a high dispersion rate and enables the dissolved residues to disperse therein. If carbon dioxide is converted to a supercritical condition, it penetrates into fine pattern portions of the object more effectively. By this feature, the additive is conveyed into pores or concave portions on a surface of the object due to the low viscosity of carbon dioxide. The carbon dioxide is pressurized to 5 MPa or more, but not less than 7.1 MPa at a temperature of 31°C to convert the carbon dioxide to a supercritical fluid condition.

[0011] Although any additives that can remove residues from microstructures could be used, it is preferred in the present invention to use quaternary ammonium fluorides because of their effective cleaning ability. The preferred fluoride compound includes at least one element selected from the group consisting of tetramethylammonium fluoride, tetraethylammonium fluoride, tetrapropylammonium fluoride, tetrabutylammonium fluoride, choline fluoride. Among these compounds, tetramethylammonium fluoride (TMAF) is the most preferable one.

[0012] If the concentration of the additive is too low, cleaning of residues is not sufficient. The lower limit of the

additive is 0.001 wt %, preferably 0.005 wt%, and more preferably 0.01 wt%. However, when the concentration is more than 0.1 wt%, low-k materials are damaged because of excessive etching of low-k materials. Thus, the upper range of the additive is 0.1 wt%, preferably 0.05 wt%, and more preferably 0.03 wt%.

[0013] The remover in the present invention also includes polyhydric alcohol. Polyhydric alcohol act as an inhibitor that protects the low-k materials from the significant damage from the additives such as fluorides. During inventors' studies, after some cleaning tests of microstructures containing of low-k films, there were some liquid-like residues. These 'liquid like residues' were recognized as byproducts originated from etching reactions between some of the compounds in the remover and a part of low-k materials. Such byproducts could not be removed and appeared as liquid-like residues because such products from low-k materials were not easily dissolved into supercritical carbon dioxide.

[0014] By further investigations, it was found that the amount of such liquid-like residues could be reduced when polyhydric alcohols were used as a component of said remover. Therefore, in the present invention, the remover includes polyhydric alcohols as an inhibitor to protect low-k materials from the damage. Although the mechanism of the protection of low-k by polyhydric alcohol is still under investigations, polyhydric alcohol might adsorb on the surface of the low-k materials and protect the surface from the attack of the chemicals.

[0015] Polyhydric alcohols may be dihydric alcohol such as ethyleneglycol, propyleneglycol, trimethyleneglycol, diethyleneglycol, dipropyleneglycol, 1,2-, 1,3-, 1,4- or 2,3-butanediol, pentamethyleneglycol, hexyleneglycol, octyleneglycol or trihydric alcohols such as glycerin, trimethylolpropanol, 1,2,6-hexanetriol, and tetrahydric alcohols such as pentaerythritol. Also, polyethyleneglycol or polypropyleneglycol may be used. Among these compounds, dihydric alcohols are preferable and ethyleneglycol and propyleneglycol are more preferable.

[0016] If the concentration of the polyhydric alcohols is too low, the protection of the low-k is not sufficient and amount of liquid-like residues increases. The lower range of the polyhydric alcohols is 0.005 wt%, preferably 0.007 wt%, and more preferably 0.01 wt%. However, when the concentration is higher than 0.1 wt%, the efficiency of the protection is saturated. Thus, the upper range of the polyhydric alcohols is 0.1 wt%, preferably 0.07 wt%, and more preferably 0.05 wt%.

[0017] As the pressurized carbon dioxide is not enough by itself to dissolve additives and inhibitors such as TMAF and polyhydric alcohols, the present invention uses co-solvent to dissolve them into carbon dioxide. The co-solvent of the present invention is a compound having an affinity to both carbon dioxide and the additive. Such a co-solvent dissolves or disperses the additive homogeneously in the pressurized carbon dioxide in fluid condition. Although any co-solvent is used if it can make additives and polyhydric alcohols soluble into pressurized carbon dioxide, alcohols are preferable. The alcohol may be any alcohol, e.g. ethanol, methanol, n-propanol, iso-propanol, n-butanol, isobutanol, diethyleneglycol monomethylether, diethyleneglycol monoethylether, and hexafluoro isopropanol. Among these alcohols, methanol, ethanol and iso-propanol are preferable because they act as a good co-solvent to wide range of compounds.

[0018] The kind and amount of the co-solvent are selected depending on the kind and amount of the additive to carbon dioxide. The amount of the co-solvent is preferably five times or more than that of the additive because the remover easily becomes homogeneous and transparent. Alternatively, the remover may include the co-solvent in a range of 1 wt. % to 50 wt. %. If more than 50 wt. % of the co-solvent is added, the penetration rate of the remover decreases due to less amount of carbon dioxide. It is preferable to use a remover including carbon dioxide, alcohol as the co-solvent, quaternary ammonium fluoride and/or quaternary ammonium hydroxide as the additive because these additives are well dissolved in carbon dioxide by alcohol and are CO_2 philic.

[0019] When TMAF is used as an additive, TMAF should be initially dissolved into said co-solvent because TMAF is a solid at ambient temperature. At this time, solvents such as dimethylacetamide (DMAC) or de-ionized water (DIW) could be added to help TMAF to be dissolved into carbon dioxide more easily. The amount of such solvents is preferably less than 20 times of TMAF. Especially, a concentration of DIW should be minimized because of the damages to the low-k materials.

[0020] The practical procedure will be described using drawings. In the below description, components of remover other than carbon dioxide, a mixture of additives, inhibitors, co-solvents is simply called 'cleaning reagents'. Figure 1 shows a simplified schematic drawing of an apparatus use for removing residues according to the present invention. In the figure, 1 is a carbon dioxide cylinder, 2 is a high pressure pump for carbon dioxide, 3 is a storage tank of cleaning reagents, 4 is a pump for cleaning reagents, 5 is a valve, 6 is a storage tank for rinse reagents, 7 is a pump for rinse reagents, 8 is a valve, 9 is a high pressure vessel, and 10 is a thermostat. Firstly, the microstructures, for example, semiconductor wafer having residues on its surface is introduced to and placed in a high pressure vessel 9, then carbon dioxide is supplied from a carbon dioxide cylinder 1 to the high pressure vessel 9 by a high pressure pump 2. The high pressure vessel 9 is thermostated at a specific temperature by a thermostat 10 in order to maintain the pressurized carbon dioxide in the high pressure vessel 9 at the supercritical condition. High pressure vessel 9 can be replaced by that having heating unit. Cleaning reagents are supplied to the high pressure vessel 9 from tanks 3 by high pressure pumps 4. Cleaning step starts at the time when the cleaning reagents are fed from tank 3 to the high pressure vessel 9. The feed of the carbon dioxide and cleaning reagents may be continuous or batch-like.

[0021] The removing process is performed at a temperature in the range from 31°C to 120°C, and at a pressure ranged from 5 M Pa to 30 M Pa, preferably, from 7.1 M Pa to 20 M Pa. The time required for removing the residues depends on the size of the object, the kind and amount of the residues, which is usually in the range from a minute to several ten minutes.

[0022] After a cleaning step, a rinse step follows. Residues removed from surface during the cleaning step remains in the vessel 9 after the cleaning step finishes. If pure carbon dioxide is fed into such conditions, some portion of residues will deposit on the surface of the objects. Therefore, after the cleaning step, the first rinse step with the mixture of carbon dioxide and rinse agents is applied. After this first rinse step, the second rinse step with pure carbon dioxide is applied.

[0023] Preferable rinse agents used in the first rinse step are those that can remove liquid-like residues. After inventors' investigations, compounds having specific dielectric constant similar to water are effective for this purpose. Since the specific dielectric constant of water is 78 at 25°C under atmospheric pressure, compounds having specific dielectric constant not smaller than 78 are used. The reason why the required specific dielectric constants are similar to that of water is that the liquid-like residues as byproducts of low-k etching have high polarity, resulting in the high affinity to the polar solvents.

[0024] On the other hand, polyhydric alcohols are required in the present invention as described in the previous section. However, if the amount of the cleaning reagents is small enough to suppress the by-production due to damages of low-k materials, rinse agent having specific dielectric constant not smaller than 78 may be used with a relative longer treatment time without any addition of polyhydric alcohols in the cleaning step. However, in order to minimize the process time of the first rinse step (for example, 5 min. or less), it is preferable to minimize the by-production of liquid-like residues with addition of polyhydric alcohols.

[0025] Practically, the first rinse step can be done by stopping the feed of the cleaning reagents by the valve 5, followed by feed of carbon dioxide and rinse reagents to the high pressure vessel 9 to get rid of the contents of vessel 9. A flow meter 12 may be used to control the flow rate. During the first rinse step, it is preferable to decrease the feed rate of rinse reagents gradually or in astepwise manner with valve 8 to replace the contents by pure carbon dioxide, followed by the second rinse step with pure carbon dioxide.

[0026] Fluid evacuated from the cleaning step and the first rinse step can be recycled and re-used by the separation into gaseous carbon dioxide and liquid fractions by a carbon dioxide recycle process, for example, including a liquid gas separator.

[0027] After the second rinse step, by releasing pressure with a pressure control valve 11, carbon dioxide vaporize to gaseous phase. Therefore, microstructures such as semiconductor wafers can be dried without any water mark and any destructions of the pattern.

[0028] Hereinafter, the present invention is described with reference to experiments. Although the present invention has been fully described by way of example with reference to the accompanying drawings, it is to be understood that various changes and modifications will be apparent to those skilled in the art. Therefore, unless otherwise such changes and modifications depart from the scope of the present invention, they should be construed as being included therein.

EXAMPLES

Example 1

[0029] At first, in order to investigate the degree of the damage of cleaning reagent to the low-k materials, etch rate measurements of low-k films were carried out. Low-k films were prepared on the silicon wafer by coating the materials consisting of organic silicon followed by heating and drying. The film thickness of the low-k films was about 5000Å and k-value was in the range of 2 to 3. Using cleaning tools shown in the figure 1, a wafer coated by the low-k film was set into the high pressure vessel 9. After closing the cover of the vessel 9, carbon dioxide was introduced from carbon dioxide cylinder 1 through the pump 2. The temperature of the vessel 9 was maintained at 50°C with a thermostat 10 and the pressure was controlled by the control valve 11. After the pressure reached 15 MPa, cleaning reagents were fed into the vessel 9 from the storage tank 4 through the pump 4. After a 10 minute-treatment, 5 minutes of the first rinse step was applied, followed by 10 minutes of the second rinse step with a pure carbon dioxide. A rinse reagent used in the first rinse step was 0.5 wt% of de-ionized water, 4.5 wt % of ethanol and 95wt% of carbon dioxide.

[0030] After the second rinse step, the pressure was released by the pressure control valve 11 and wafer was taken to be provided for further evaluation. Etch rates (Å/min) were calculated by the difference in the film thickness before and after the treatment divided by the 10 min. Film thickness was measured by an optical measurement tool. The results are shown in table 1.

[0031] The abbreviation used in table 1 are follows;

[0032] TMAF: Tetramethylammoniumfluoride, DMAC: Dimethylacetamide, DIW: de-ionized water, EG: Ethyleneglycol, PG: Propyleneglycol, EtOH: Ethanol

Table 1

| Run - | Componets of remover | | | | | | | Etch rate Å/min |
|-------|----------------------|------------------------|-------|-------|------------|---------------------|-------|-----------------|
| | CO ₂ | Additive and inhibitor | | | Co-solvent | Additional solvents | | |
| | | TMAF | EG | PG | EtOH | DMAC | DIW | |
| 1 | 95 | 0.013 | 0 | 0 | 4.9 | 0.063 | 0.024 | 240 |
| 2 | 95 | 0.013 | 0.012 | 0 | 4.9 | 0.051 | 0.024 | 230 |
| 3 | 95 | 0.013 | 0 | 0.012 | 4.9 | 0.063 | 0.024 | 155 |
| 4 | 95 | 0.013 | 0 | 0.024 | 4.9 | 0.051 | 0.024 | 148 |
| 5 | 95 | 0.005 | 0 | 0 | 5.1 | 0.066 | 0 | 53 |
| 6 | 95 | 0.005 | 0 | 0.012 | 4.9 | 0.054 | 0 | 19 |
| 7 | 95 | 0.013 | 0 | 0 | 4.8 | 0.165 | 0 | 91 |
| 8 | 95 | 0.013 | 0 | 0.03 | 4.8 | 0.135 | 0 | 67 |

Example 2

[0033] In the same manner described in the example 1, wafers coated by the low-k film were prepared. After line and space patterns (180 nm width) were processed by the lithography on the surface, ordinary etching by fluorocarbon gases and ashing by oxygen plasma. After one minute cleaning with cleaning reagents listed in the table 2 under the same condition as the example 1, five minute or ten minute of the first rinse step using components listed in table 2, followed by ten minutes of the second rinse step with a pure carbon dioxide. The first rinse reagents used were 0.5 wt% of listed components, 4.5 wt% of ethanol and 95 wt% of carbon dioxide. After the release of the pressure by opening the pressure control valve 11, the treated wafer was taken and provided for the evaluation. The cleaning performance was evaluated by the observation of a scanning electron microscope (SEM) with amplitude of 50000. The performance was checked both residues on the surface of the line and the liquid-like residues. The criteria used for investigation was as follows;

[0034] Excellent: No residues remained

[0035] Good: Amount of residues was less than 1 area % on the patterned side of the wafer.

[0036] NG (Not good): Amount of residues was more than 1 area %.

[0037] The abbreviation used in table 2 are follows;

[0038] TMAF: Tetramethylammoniumfluoride, DMAC: Dimethylacetamide, H₂O: water ($\epsilon=78$), DIW: de-ionized water, EG: Ethyleneglycol, PG: Propyleneglycol, EtOH: Ethanol, FA: Formamide ($\epsilon=111$), MF: Methylformamide ($\epsilon=182$), DMF: Dimethylformamide ($\epsilon=36.7$), MeOH: Methanol ($\epsilon=42$), AC: Acetone ($\epsilon=21$)

[0039] According to the cleaning process described in the present invention, low-k materials that are easily damaged by the cleaning reagents could be protected by the use of the cleaning reagents including inhibitors such as polyhydric alcohols added into carbon dioxide. Besides, residues produced because of the damages of low-k materials by the cleaning reagents could be removed by a suitable selection of the rinse reagents. Therefore, the cleaning process described in the present invention provides one of the optimized cleaning processes applicable to the microstructure such as semiconductor wafers.

Table 2

| Run | Components of remover | | | | | | | | | | Rinse | 1 min cleaning + 5 min 1st rinse | | 1 min cleaning + 10 min 1st rinse | |
|-----|-----------------------|------------------------|-------|-------|------------|---------------------|-------|------------------|-------------|-----------|-----------|-------------------------------------|-----------|--------------------------------------|--|
| | CO ₂ | Additive and inhibitor | | | Co-solvent | Additional solvents | | | liquid-like | polymer | | liquid-like | polymer | | |
| | | TMAF | EG | PG | | EtOH | DMAC | DIW | | | | | | | |
| | | | | | | | | | | | | | | | |
| 1 | 95 | 0.013 | 0 | 0 | 4.9 | 0.063 | 0.024 | DMF | NG | Excellent | NG | polymer | Excellent | | |
| 2 | 95 | 0.013 | 0 | 0 | 4.9 | 0.063 | 0.024 | MeOH | NG | Excellent | NG | Excellent | Excellent | | |
| 3 | 95 | 0.013 | 0 | 0 | 4.9 | 0.063 | 0.024 | AC | NG | Excellent | NG | Excellent | Excellent | | |
| 4 | 95 | 0.013 | 0 | 0 | 4.9 | 0.063 | 0.024 | H ₂ O | NG | Excellent | Excellent | Excellent | Excellent | | |
| 5 | 95 | 0.013 | 0 | 0 | 4.9 | 0.063 | 0.024 | FA | Excellent | Excellent | Excellent | Excellent | Excellent | | |
| 6 | 95 | 0.013 | 0 | 0 | 4.9 | 0.063 | 0.024 | MF | Excellent | Excellent | Excellent | Excellent | Excellent | | |
| 7 | 95 | 0.013 | 0.012 | 0 | 4.9 | 0.051 | 0.024 | H ₂ O | NG | Excellent | Excellent | Excellent | Excellent | | |
| 8 | 95 | 0.013 | 0 | 0.012 | 4.9 | 0.063 | 0.024 | H ₂ O | Good | Excellent | Excellent | Excellent | Excellent | | |
| 9 | 95 | 0.013 | 0 | 0.012 | 4.9 | 0.063 | 0.024 | FA | Excellent | Excellent | Excellent | Excellent | Excellent | | |
| 10 | 95 | 0.013 | 0 | 0.024 | 4.9 | 0.051 | 0.024 | H ₂ O | Excellent | Excellent | Excellent | Excellent | Excellent | | |
| 11 | 95 | 0.005 | 0 | 0 | 5.1 | 0.066 | 0 | H ₂ O | Good | Good | Excellent | Good | Good | | |
| 12 | 95 | 0.005 | 0 | 0.012 | 4.9 | 0.054 | 0 | H ₂ O | Excellent | Good | Excellent | Good | Good | | |
| 13 | 95 | 0.013 | 0 | 0 | 4.8 | 0.165 | 0 | H ₂ O | Good | Excellent | Excellent | Excellent | Excellent | | |
| 14 | 95 | 0.013 | 0 | 0 | 4.8 | 0.165 | 0 | FA | Excellent | Excellent | Excellent | Excellent | Excellent | | |
| 15 | 95 | 0.013 | 0 | 0.03 | 4.8 | 0.135 | 0 | H ₂ O | Excellent | Excellent | Excellent | Excellent | Excellent | | |

Claims

1. A process for removing residues from the microstructure of an object comprising steps of:
 - 5 preparing a remover including carbon dioxide, an additive for removing the residues, an inhibitor for suppressing residues and a co-solvent for dissolving said additive and said inhibitor in said carbon dioxide at a pressurized fluid condition; and
bringing the object into contact with said remover so as to remove the residues from the object.
- 10 2. The process according to claim 1, wherein said additive includes quaternary ammonium fluoride.
3. The process according to claim 1, wherein said additive includes tetramethylammonium fluoride.
4. The process according to claim 1, 2 or 3, wherein the concentration of said additive is between 0.001 to 0.1 weight percent.
- 15 5. The process according to anyone of claims 1 to 4, wherein said inhibitor includes polyhydric alcohol.
6. The process according to claim 5, wherein said polyhydric alcohol is a dihydric alcohol.
- 20 7. The process according to claim 5 or 6, wherein said dihydric alcohol is a propylene glycol.
8. A process for removing residues from the microstructure of an object comprising steps of:
 - 25 preparing a remover including carbon dioxide, an additive for removing the residues and a co-solvent for dissolving said additive in said carbon dioxide at a pressurized fluid condition; and
bringing the object into contact with said remover so as to remove the residues from the object followed by a rinse step including rinse agent of which dielectric constant at a temperature and pressure of 25°C and 1 atm is 78 or larger.
- 30 9. The process according to claim 8, wherein said rinse agent is selected from at least one of the compounds including water, formamide, methylformamide and methylacetamide.
10. The process according to claim 8 or 9, wherein said remover includes an inhibitor for suppressing residues.
- 35 11. The process according to claim 8, 9 or 10, wherein said additive includes quaternary ammonium fluoride.
12. The process according to claim 8, 9 or 10, wherein said additive includes tetramethylammonium fluoride.
- 40 13. The process according to anyone of claims 8 to 12, wherein the concentration of said additive is between 0.001 to 0.1 weight percent.
14. The process according to anyone of claims 10 to 13, wherein said inhibitor includes polyhydric alcohol.
- 45 15. The process according to claim 14, wherein said polyhydric alcohol is a dihydric alcohol.
16. The process according to claim 14, wherein said dihydric alcohol is a propylene glycol.
17. A composition for removing residue from the microstructure of an object, comprising
 - 50 carbon dioxide, a fluoride containing additive, a co-solvent or mixture of co-solvents capable of dissolving the fluoride containing additive, and an inhibitor.
18. The composition according to claim 17, wherein the fluoride containing additive is a quaternary ammonium fluoride.
- 55 19. The composition according to claim 18, wherein the quaternary ammonium fluoride is tetramethylammonium fluoride.

EP 1 365 441 A1

20. The composition according to claim 17, 18 or 19, wherein the co-solvent or mixture of co-solvents is ethanol, methanol, n-propanol, isopropanol, n-butanol or dimethylacetamide.

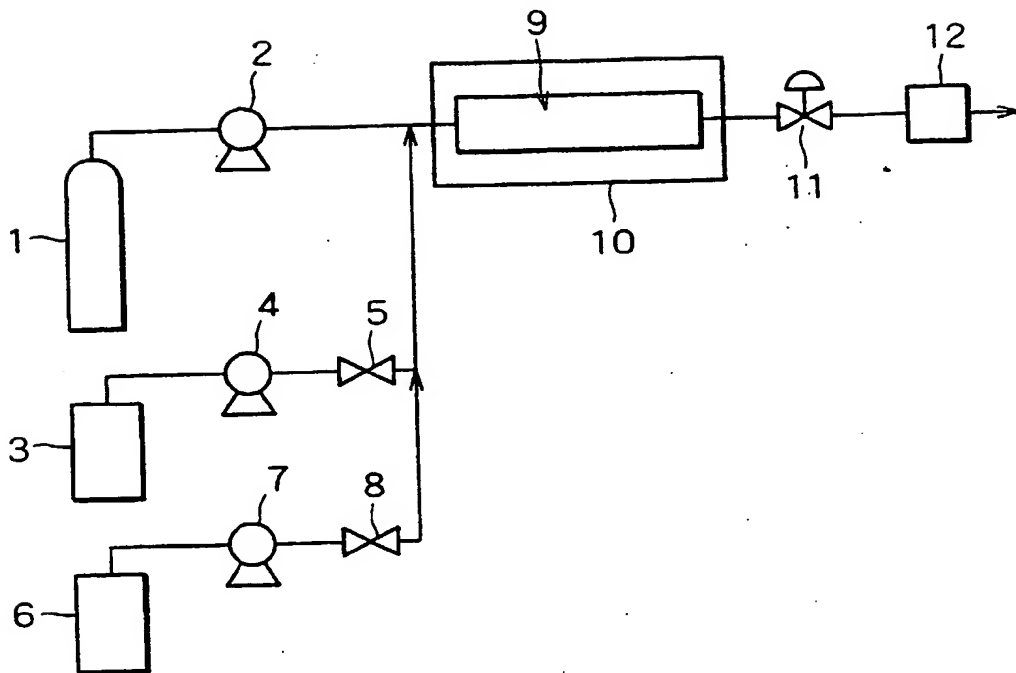
5 21. The composition according to claim 20, wherein the co-solvent is a mixture of ethanol and dimethylacetamide.

22. The composition according to anyone of claims 17 to 21, wherein the inhibitor is propylene glycol.

23. A composition for removing residue from the microstructure of an object, comprising

10 carbon dioxide, tetramethylammoniumfluoride, ethanol, dimethylacetamide, and propylene glycol.

FIG. 1





European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 03 01 1130

| DOCUMENTS CONSIDERED TO BE RELEVANT | | | |
|---|---|--|--|
| Category | Citation of document with indication, where appropriate, of relevant passages | Relevant to claim | CLASSIFICATION OF THE APPLICATION (Int.Cl.7) |
| P, A | US 2002/164873 A1 (KAWAKAMI NOBUYUKI ET AL) 7 November 2002 (2002-11-07) * claims 1-20 * | 1-23 | H01L21/00 B08B7/00 G03F7/42 C11D11/00 C11D7/32 |
| A | US 6 306 564 B1 (MULLEE WILLIAM H) 23 October 2001 (2001-10-23) * claims 1-57 * | 1-23 | |
| A | WO 02 15251 A (TOKYO ELECTRON LTD) 21 February 2002 (2002-02-21) * claims 1-43 * | 1-23 | |
| A | WO 01 33613 A (SUPERCritical SYSTEMS INC) 10 May 2001 (2001-05-10) * claims 1-35 * | 1-23 | |
| P, A | WO 02 080233 A (KAWAKAMI NOBUYUKI; YAMAGATA MASAHIRO (JP); SUZUKI TETSUO (JP); EGB) 10 October 2002 (2002-10-10) * claims 1-20 * | 1-23 | |
| | | | TECHNICAL FIELDS SEARCHED (Int.Cl.7) |
| | | | H01L B08B G03F C11D |
| The present search report has been drawn up for all claims | | | |
| Place of search THE HAGUE | | Date of completion of the search 28 July 2003 | Examiner Richards, M |
| CATEGORY OF CITED DOCUMENTS | | T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date O : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document | |
| X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document | | | |

EPO FORM 1503 (03.02) (P4/C01)

**ANNEX TO THE EUROPEAN SEARCH REPORT
ON EUROPEAN PATENT APPLICATION NO.**

EP 03 01 1130

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on
The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

28-07-2003

| Patent document cited in search report | Publication date | Patent family member(s) | Publication date |
|---|---------------------|----------------------------|---------------------|
| US 2002164873 A1 | 07-11-2002 | JP 2002237481 A | 23-08-2002 |
| | | WO 02080233 A2 | 10-10-2002 |
| | | US 2003106573 A1 | 12-06-2003 |
| US 6306564 B1 | 23-10-2001 | US 2003027085 A1 | 06-02-2003 |
| | | US 2002048731 A1 | 25-04-2002 |
| | | US 6500605 B1 | 31-12-2002 |
| WO 0215251 A | 21-02-2002 | WO 0215251 A1 | 21-02-2002 |
| | | AU 6644200 A | 25-02-2002 |
| | | EP 1309990 A1 | 14-05-2003 |
| WO 0133613 A | 10-05-2001 | US 6500605 B1 | 31-12-2002 |
| | | AU 1455001 A | 14-05-2001 |
| | | CA 2387334 A1 | 10-05-2001 |
| | | CN 1384972 T | 11-12-2002 |
| | | EP 1226603 A2 | 31-07-2002 |
| | | JP 2003513342 T | 08-04-2003 |
| | | TW 500985 B | 01-09-2002 |
| | | WO 0133613 A2 | 10-05-2001 |
| WO 02080233 A | 10-10-2002 | JP 2002237481 A | 23-08-2002 |
| | | WO 02080233 A2 | 10-10-2002 |
| | | US 2002164873 A1 | 07-11-2002 |
| | | US 2003106573 A1 | 12-06-2003 |

EPO FORM P4459

For more details about this annex : see Official Journal of the European Patent Office, No. 12/82

THIS PAGE BLANK (USPTO)